

Fully Probabilistic Design of LQ Control with On-Line Parameter Tuning

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Outline:**Intro**FPD**C**

Model

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Tuning

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Fully Probabilistic Design of LQ Control with On-Line Parameter Tuning

Outline:

- ① Intro Motivation, Purpose, Ideological line
- ② FPD**C** Fully Probabilistic Design of Control
- ③ Model Probabilistic model representation
- ④ Im**P**D Implementation of Probabilistic Design
- ⑤ Tuning On-line Fully Probabilistic Tuning of C.
- ⑥ Exmpl Application examples
- ⑦ Concl. Conclusion



① Intro: Motivation, Purpose, Ideological line

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Motivation I.

To design several simple general algorithms for control of class of mechatronic systems (e.g. robotic tools) influenced by uncertain neighborhood interactions both of known and unknown source.

Motivation II.

To understand fundamentals of software tools developed in our department.

Starting informational sources:

design and algorithms of adaptive LQ Control >> Josef Böhm

fully probabilistic theory used in control design >> Miroslav Karný

1 Intro: Motivation, Purpose, Ideological line

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Block representation of system and its neighborhood

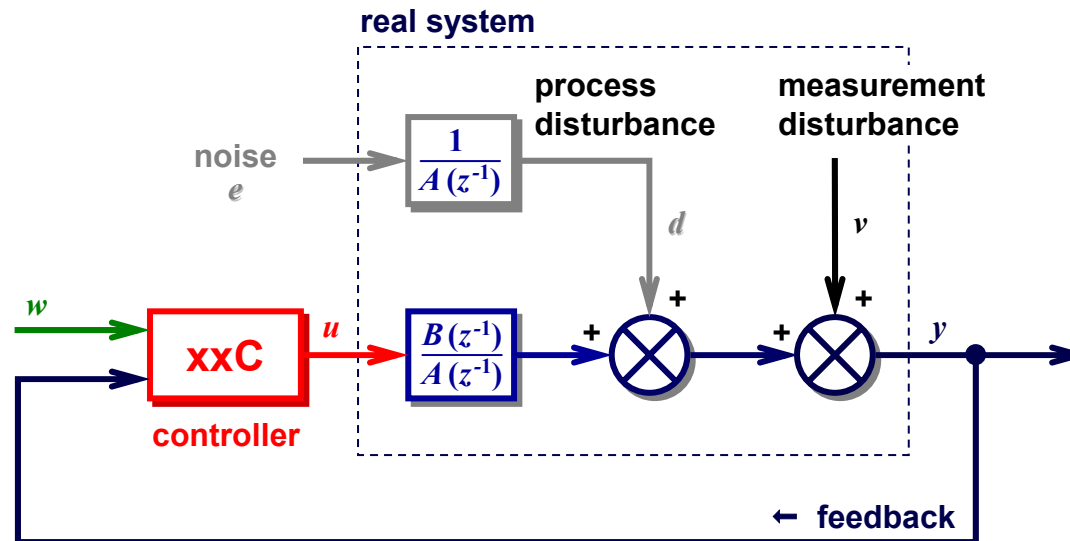


diagram of closed-loop

Main purpose:

To test the different control strategies (LQ Control strategy designed by probabilistic theory is one of them) for selection of suitable control for mechatronic and robotic applications.



1 Intro: Motivation, Purpose, Ideological line

Theory >> Practice

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Theory: Fully Probabilistic Design (FPD) of Control

- general case:

$$J = J(\underbrace{pdf}_{\text{criterion}}, \underbrace{lpdf}_{\text{model}}) \quad \underbrace{\min_{pdf} J}_{\text{minimization}} \quad \underbrace{o pdf}_{\text{opt. control}}$$

>> criterion + model >> minimization >> opt. control

- specific case:

>> FPD of Control leads to standard LQ Control, i.e. FPD gives new interpretation to LQ Control e.g. a possibility to on-line "fine - tune" or "retune" LQ Controller in view of uncertain neighborhood interactions.

Practice (practical use):

special algorithms for specific FPD need not be designed; standard LQ Control algorithms can be utilized, due to probabilistic interpretation, with specific tuning.

② FPD_{of}C: Fully Probabilistic Design of Control

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Criterion:

$$\mathcal{D}(f \parallel {}^I f) \equiv E \left\{ \ln \left(\frac{f(X)}{{}^I f(X)} \right) \right\} = \int f(X) \ln \left(\frac{f(X)}{{}^I f(X)} \right) dX$$

Kullback-Leibler divergence (*KL-divergence*) measures proximity of real and ideal distributions of closed-loop

- joint *pdf* representing the real closed-loop behavior:

$$f(X) = f_N \equiv f(\mathbf{x}_{k+N}, u_{k+N-1}, \mathbf{x}_{k+N-1}, u_{k+N-2}, \dots, u_k, \mathbf{x}_k)$$

$$\text{assuming} = \left\{ \prod_{j=k+1}^{k+N} f(\mathbf{x}_j | \mathbf{x}_{j-1}, u_{j-1}) f(u_{j-1} | \mathbf{x}_{j-1}) \right\} f(\mathbf{x}_k)$$

- joint *pdf* representing the ideal closed-loop behavior:

$${}^I f(X) = {}^I f_N \equiv {}^I f(\mathbf{x}_{k+N}, u_{k+N-1}, \mathbf{x}_{k+N-1}, u_{k+N-2}, \dots, u_k, \mathbf{x}_k)$$

$$\text{assuming} = \left\{ \prod_{j=k+1}^{k+N} {}^I f(\mathbf{x}_j | \mathbf{x}_{j-1}, u_{j-1}) {}^I f(u_{j-1} | \mathbf{x}_{j-1}) \right\} f(\mathbf{x}_k)$$

2 FPD^{of}C: Fully Probabilistic Design of Control

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Task specification:

$$\{ {}^O f(u_{j-1} | \mathbf{x}_{j-1}) \}_{j=k+1}^{k+N} \in \arg \min_{\{ f(u_{j-1} | \mathbf{x}_{j-1}) \}_{j=k+1}^{k+N}} \mathcal{D}(f_N \| {}^I f_N)$$

Minimization procedure in brief:

$$\min_{\{ f(u_{j-1} | \mathbf{x}_{j-1}) \}_{j=k+1}^{k+N}} \mathcal{D}(f_N \| {}^I f_N) = \min_{\{ f(u_{j-1} | \mathbf{x}_{j-1}) \}_{j=k+1}^{k+N}} E \sum_{j=k+1}^{k+N} z_j = \dots$$

$$= \min_{\{ f(u_k | \mathbf{x}_k) \}} \left\{ E(z_{k+1}) + \dots \min_{\{ f(u_{k+N-2} | \mathbf{x}_{k+N-2}) \}} \left\{ E(z_{k+N-1}) + \min_{\{ f(u_{k+N-1} | \mathbf{x}_{k+N-1}) \}} \{ E(z_{k+N}) \} \right\} \dots \right\}$$

dynamic programming

$$z_j = \ln \frac{f(\mathbf{x}_j | \mathbf{x}_{j-1}, u_{j-1}) f(u_{j-1} | \mathbf{x}_{j-1})}{{}^I f(\mathbf{x}_j | \mathbf{x}_{j-1}, u_{j-1}) {}^I f(u_{j-1} | \mathbf{x}_{j-1})} = j^{th} \text{ partial loss}$$

⇒ Optimal control pdf

② FPD_{of}C: Fully Probabilistic Design of Control

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Optimal control pdf

$${}^o f(u_{j-1} | \mathbf{x}_{j-1}) = \frac{1}{\gamma(\mathbf{x}_{j-1})} {}^I f(u_{j-1} | \mathbf{x}_{j-1}) e^{-\delta(u_{j-1}, \mathbf{x}_{j-1})}$$

where factors δ and γ are defined as follows:

$$\delta(u_{j-1}, \mathbf{x}_{j-1}) \equiv \int f(\mathbf{x}_j | u_{j-1}, \mathbf{x}_{j-1}) \ln \left(\frac{f(\mathbf{x}_j | u_{j-1}, \mathbf{x}_{j-1})}{\gamma(\mathbf{x}_j) {}^I f(\mathbf{x}_j | u_{j-1}, \mathbf{x}_{j-1})} \right) d\mathbf{x}_j$$

$$\gamma(\mathbf{x}_{j-1}) \equiv \int {}^I f(u_{j-1} | \mathbf{x}_{j-1}) e^{-\delta(u_{j-1}, \mathbf{x}_{j-1})} du_{j-1}$$

The factors are expressed recursively.

They are set up on the basis of minimization procedure.

③ Model: Probabilistic model representation

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$$\mathcal{N}(\mu_y, \sigma_y^2) \equiv \mathcal{N}(\mu_y, r_y): f(y) = \frac{1}{\sigma_y \sqrt{2\pi}} e^{-\frac{(y-\mu_y)^2}{2\sigma_y^2}} \equiv \frac{1}{\sqrt{2\pi r_y}} e^{-\frac{(y-\mu_y)^2}{2r_y}}$$

ARX

$$\text{model: } y_k = \underbrace{\sum_{i=1}^n b_i u_{k-i} - \sum_{i=1}^n a_i y_{k-i}}_{\mu_y} + e_{y_k}, \quad e_{y_k} \sim \mathcal{N}(0, r_y)$$

State-Space

$$\text{model: } \mathbf{x}_{k+1} = \mathbf{A} \mathbf{x}_k + \mathbf{B} u_k + \mathbf{e}_{\mathbf{x}_{k+1}}, \quad \mathbf{e}_{\mathbf{x}_{k+1}} \sim \mathcal{N}(\mathbf{0}, \mathbf{R})$$

$$y_k = \mathbf{C} \mathbf{x}_k$$

$$y_k = \underbrace{\mathbf{C} \mathbf{A} \mathbf{x}_{k-1} + \mathbf{C} \mathbf{B} u_{k-1}}_{\mu_y} + \underbrace{\mathbf{C} \mathbf{e}_{\mathbf{x}_k}}_{e_{y_k}}, \quad e_{y_k} \sim \mathcal{N}(0, r_y) = \mathcal{N}(0, \mathbf{C} \mathbf{R} \mathbf{C}^T)$$

$$\mathbf{x}_k = \begin{bmatrix} u_{k-1} \\ \vdots \\ u_{k-n+1} \\ y_k \\ \vdots \\ y_{k-n+1} \end{bmatrix} \quad \mathbf{A} = \begin{bmatrix} 0 & \cdots & 0 & 0 & \cdots & 0 \\ \vdots & \ddots & \vdots & \vdots & \ddots & \vdots \\ 0 & \cdots & 0 & 0 & \cdots & 0 \\ b_2 & \cdots & b_n & -a_1 & \cdots & -a_n \\ 0 & \cdots & 0 & 1 & \cdots & 0 \\ 0 & \ddots & 0 & 0 & \ddots & 0 \end{bmatrix} \quad \mathbf{B} = \begin{bmatrix} 1 \\ \vdots \\ 0 \\ b_1 \\ \vdots \\ 0 \end{bmatrix} \quad \mathbf{C} = \begin{bmatrix} 0 \\ \vdots \\ 0 \\ 1 \\ \vdots \\ 0 \end{bmatrix}^T \quad \mathbf{e}_{\mathbf{x}_k} = \begin{bmatrix} 0 \\ \vdots \\ 0 \\ 1 \\ \vdots \\ 0 \end{bmatrix} e_{y_k}$$

4 Im^{of}PD: Implementation of Probabilistic Design

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Im^{of}PD
=
evaluation:

$$\left\{ \begin{array}{l} {}^o f(u_{j-1} | \mathbf{x}_{j-1}) = \frac{1}{\gamma(\mathbf{x}_{j-1})} {}^I f(u_{j-1} | \mathbf{x}_{j-1}) e^{-\delta(u_{j-1}, \mathbf{x}_{j-1})} \\ \gamma(\mathbf{x}_{j-1}) = fce(f(\mathbf{x}_j | u_{j-1}, \mathbf{x}_{j-1}), {}^I f(u_{j-1} | \mathbf{x}_{j-1}), \delta(u_{j-1}, \mathbf{x}_{j-1})) \\ \delta(u_{j-1}, \mathbf{x}_{j-1}) = fce(f(\mathbf{x}_j | u_{j-1}, \mathbf{x}_{j-1}), {}^I f(\mathbf{x}_j | u_{j-1}, \mathbf{x}_{j-1}), \gamma(\mathbf{x}_j)) \end{array} \right.$$

- *pdf* of the **real** controlled system **state** behavior: $f(\mathbf{x}_j | u_{j-1}, \mathbf{x}_{j-1}) = \dots$
+ system state-space model: $\mu_y = \mathbf{C}\mu_x = \mathbf{C}\mathbf{A}\mathbf{x}_{j-1} + \mathbf{C}\mathbf{B}u_{j-1}$
- *pdf* of the **ideal** controlled system **state** behavior: ${}^I f(\mathbf{x}_j | u_{j-1}, \mathbf{x}_{j-1}) = \dots$
+ j^{th} user ideal (i.e. desired values): ${}^I y_j = \mathbf{C}^I \mu_x = {}^I \mu_y = w_j$
- *pdf* of the **ideal** controlled system **input** behavior: ${}^I f(u_{j-1} | \mathbf{x}_{j-1}) = \dots$
+ value of system input ideal: ${}^I u_{j-1} = {}^I \mu_u = u_{j-2}$
- ⇒ *pdf* of the **optimal** (designed) controlled system **input** behavior:
 ${}^o f(u_k | \mathbf{x}_k) = \dots, {}^o u_k = \dots$

4 ImPC: Implementation of Probabilistic Design

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- *pdf* of the **real** controlled system **output** behavior:

$$f(\mathbf{C}\mathbf{x}_{k+1} | u_k, \mathbf{x}_k) = \frac{1}{\sqrt{2\pi r_y}} e^{-\frac{1}{2}(\mathbf{C}\mathbf{x}_{k+1} - \mathbf{C}\mu_x)^T r_y^{-1} (\mathbf{C}\mathbf{x}_{k+1} - \mathbf{C}\mu_x)}$$

- *pdf* of the **ideal** controlled system **output** behavior:

$$^I f(\mathbf{C}\mathbf{x}_{k+1} | u_k, \mathbf{x}_k) = \frac{1}{\sqrt{2\pi r_y}} e^{-\frac{1}{2}(\mathbf{C}\mathbf{x}_{k+1} - w_{k+1})^T r_y^{-1} (\mathbf{C}\mathbf{x}_{k+1} - w_{k+1})}$$

- *pdf* of the **ideal** controlled system **input** behavior:

$$^I f(u_k | \mathbf{x}_k) = \frac{1}{\sqrt{2\pi {}^I r_u}} e^{-\frac{1}{2}(u_k - u_{k-1})^T r_u^{-1} (u_k - u_{k-1})}$$

- ⇒ *pdf* of the **optimal** (designed) controlled system **input** behavior:

$$^o f(u_k | \mathbf{x}_k) = \frac{1}{\sqrt{2\pi {}^o r_u}} e^{-\frac{1}{2} {}^o r_u^{-1} \{u_k + k_x \mathbf{x}_k - \sum_{j=k+1}^{k+N+1} k_{w_j} w_j - k_u u_{k-1}\}^2}$$

$$^o u_k = -k_x \mathbf{x}_k + \sum_{j=k+1}^{k+N+1} k_{w_j} w_j + k_u u_{k-1}$$

Note:

This result
is equivalent
to standard
LQ Control.

5 Tuning: On-line Fully Probabilistic Tuning of C.

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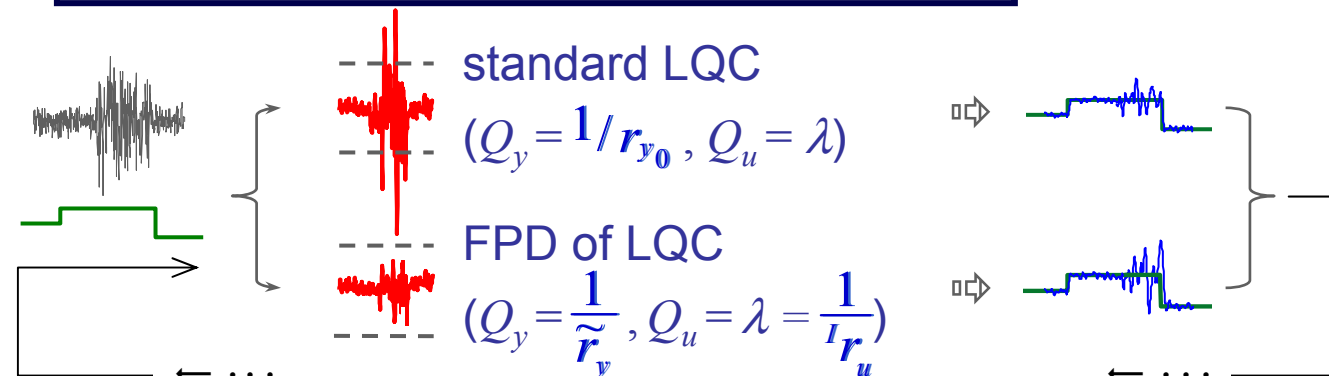
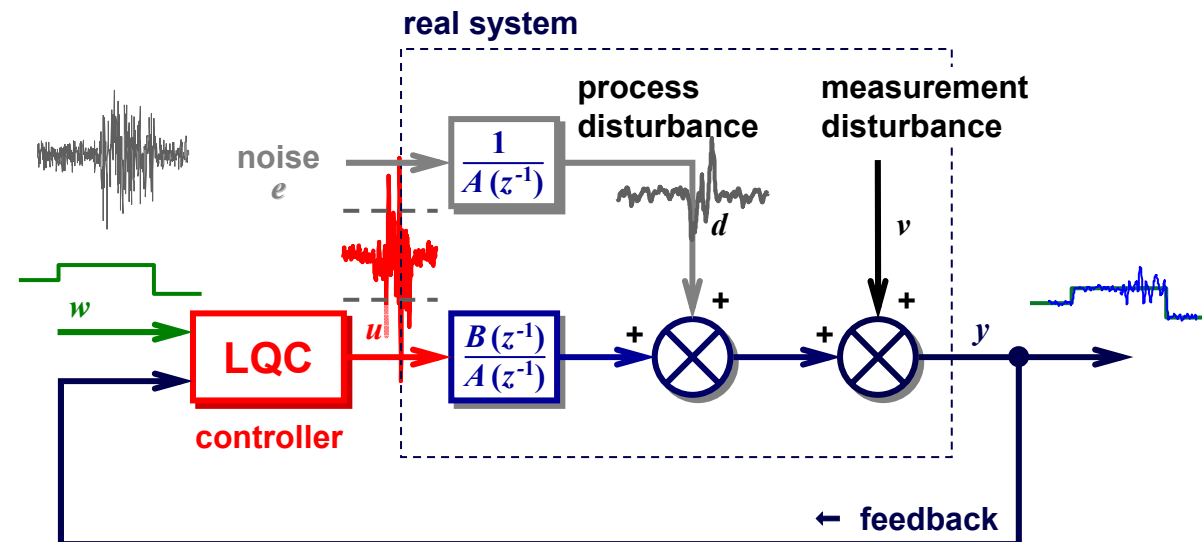
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Case specification, in which the on-line tuning is desirable:
Real control of real system in real environment (i.e. real conditions causing interference occurred randomly in control process).



5 Tuning: On-line Fully Probabilistic Tuning of C.

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Quadratic criterion used in LQ Control design:

$$J = \sum_{j=k}^{k+N} \left((\hat{y}_{j+1} - \overset{I\mu_y}{w_{j+1}})^T Q_y (\hat{y}_{j+1} - w_{j+1}) + (u_j - \overset{I\mu_u}{u_{j-1}})^T Q_u (u_j - u_{j-1}) \right)$$

standard LQC ($Q_y = \mathbf{1}/r_{y_0}$, $Q_u = \lambda$), FPD of LQC ($Q_y = \frac{1}{\tilde{r}_y}$, $Q_u = \lambda = \frac{1}{I r_u}$)

where r_y or practically $\hat{r}_{y_i} = \hat{e}_{y_i} \hat{e}_{y_i}^T$, which is very changeable $\Rightarrow$ filtration $\hat{r}_{y_i}$ suitable filter -

- exponential forgetting:

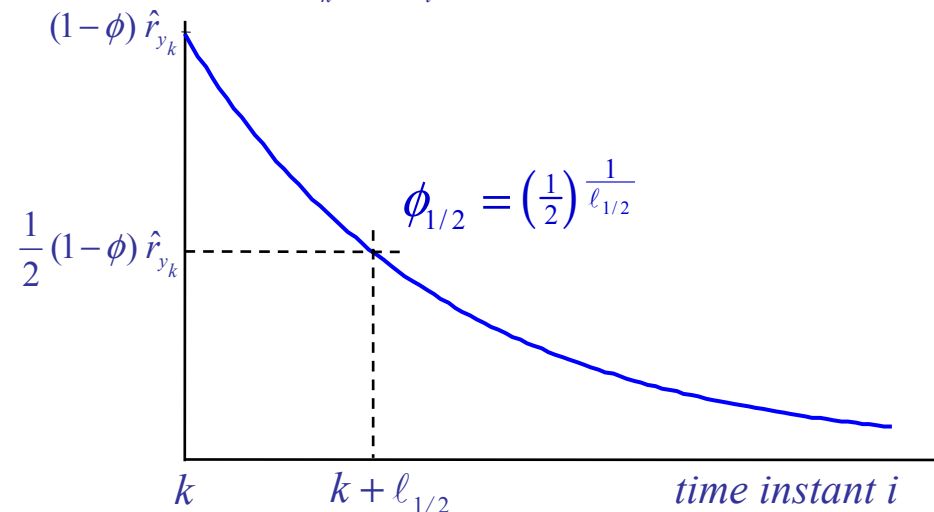
$$\tilde{r}_{y_1} = (1 - \phi) \hat{r}_{y_1}$$

$$\tilde{r}_{y_i} = \phi \tilde{r}_{y_{i-1}} + (1 - \phi) \hat{r}_{y_i}$$

$$i = 2, \dots, k$$

$$\tilde{r}_{y_k} = (1 - \phi) \sum_{i=1}^k \phi^{k-i} \hat{r}_{y_i}$$

contribution of $\hat{r}_{y_k}$ to $\tilde{r}_{y_i}$



6 Exmpl: Application examples

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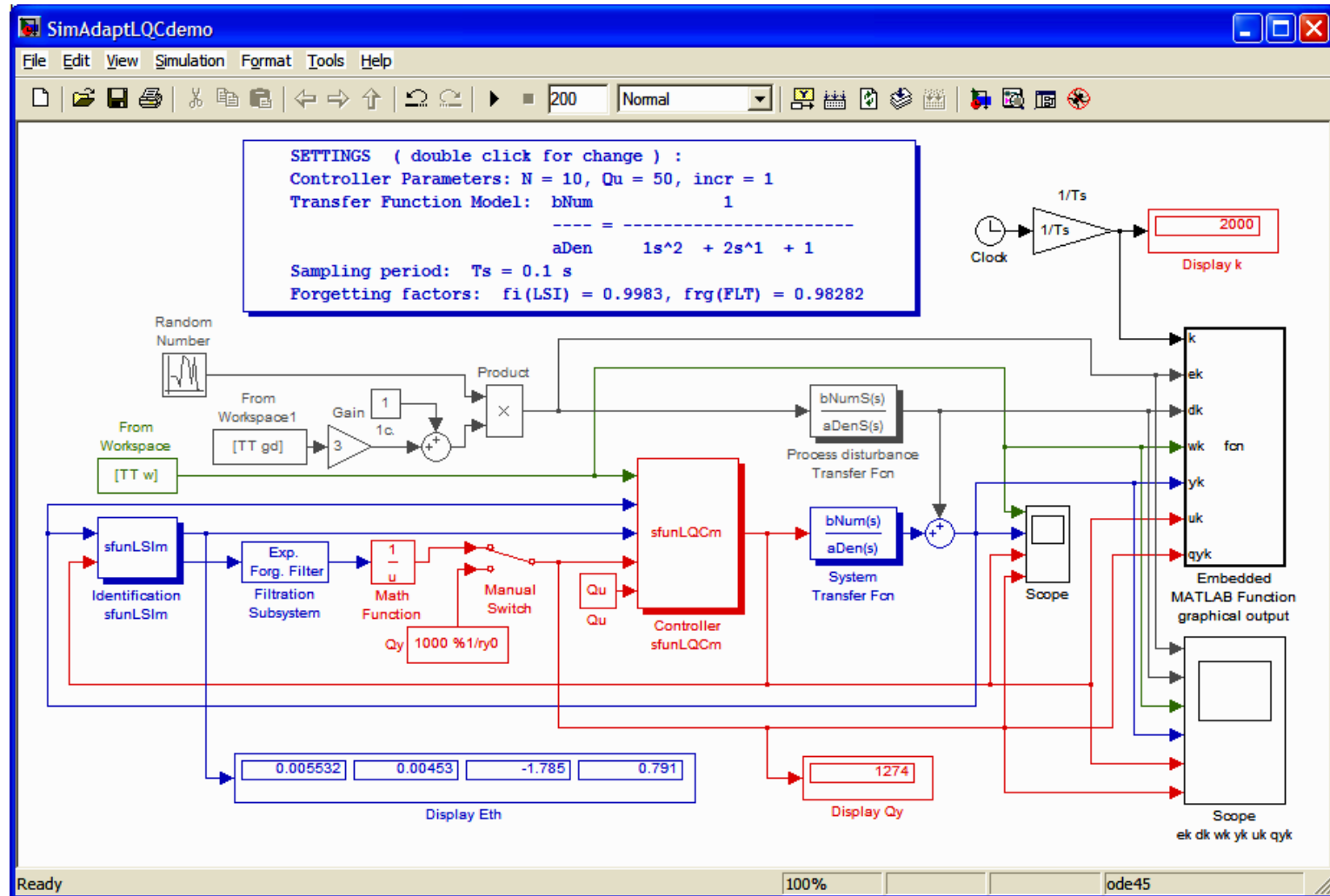
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⑥ Exmpl: Application examples

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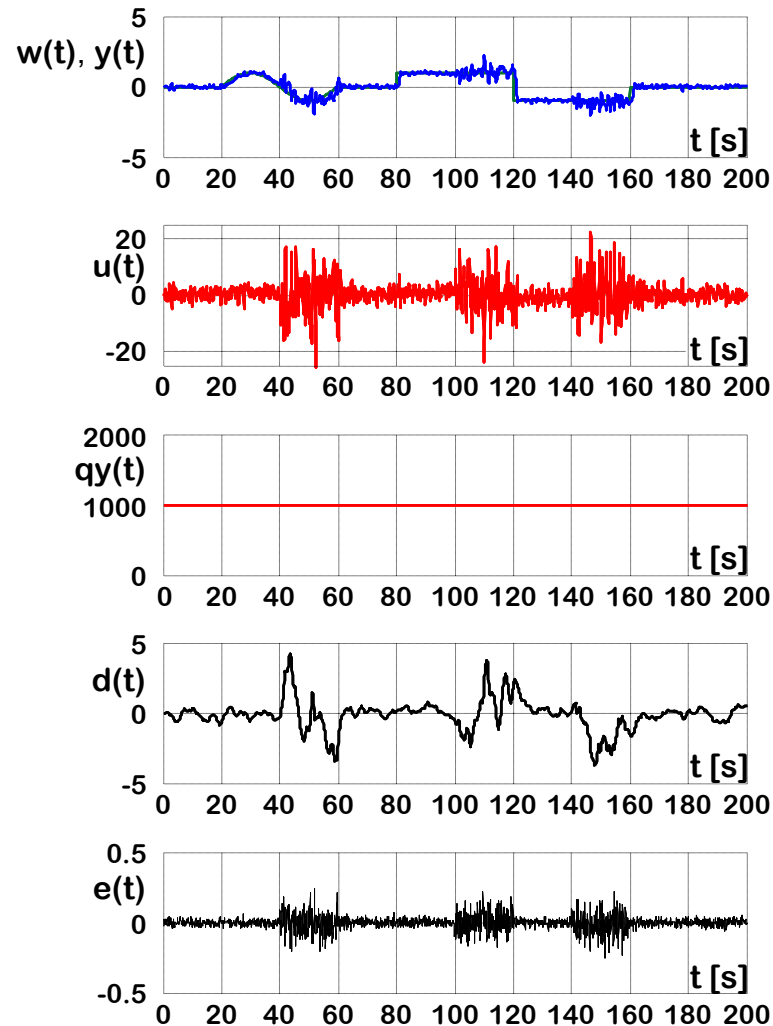
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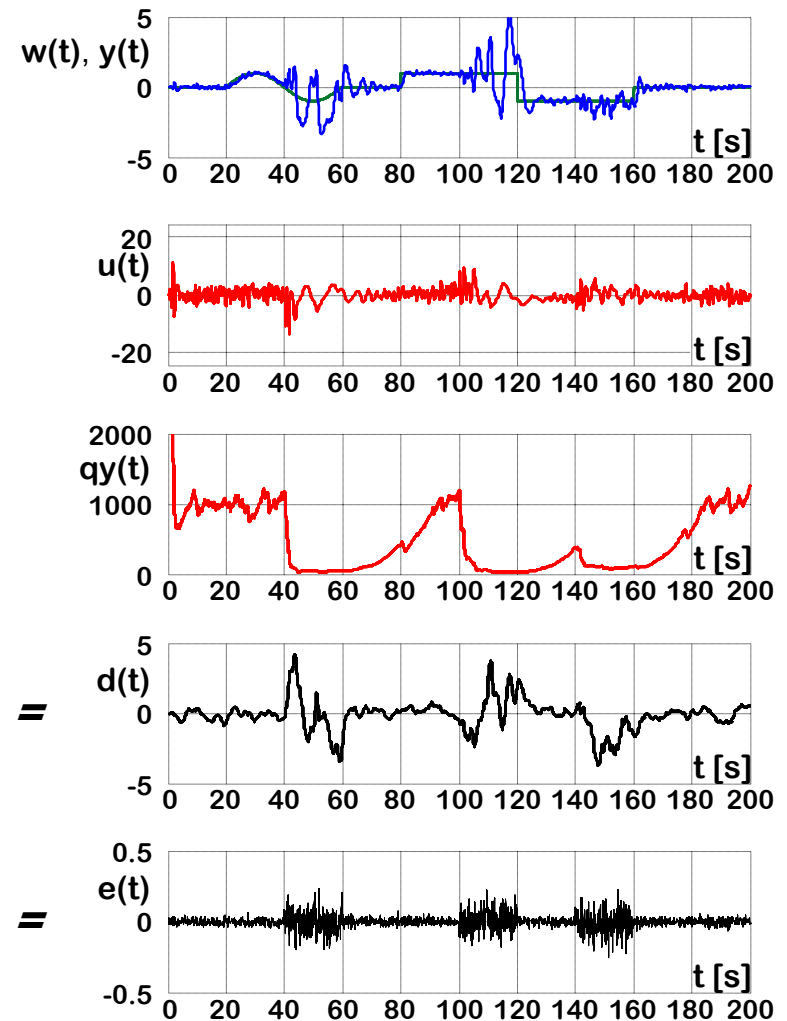
Exmpl

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standard LQC ($Q_y = 1/r_{y0}$, $Q_u = \lambda$)



FPD of LQC ($Q_y = 1/\tilde{r}_y$, $Q_u = \lambda = 1/r_u$)



7 Concl.: Conclusion

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Several concluding comments

on drawbacks:

- difficult derivation caused by **complicated notation**
(a lot of different parameters/factors in complicated expressions)
- **difficult initial** parameter/factor **determination**
(various methods of mathematical-physical identification/analysis are needed)
- **assumption of specific distributions** of the closed-loop variables, which enables this design to be computed, **is a limiting factor**

on benefits:

- enable designer to use **detailed** closed-loop **description**
- fully probabilistic interpretation of **LQ Control parameters** enabling users to **self-fine-tune or retune** these parameters
- potential use of parameter **fine-tuning or retuning** in advanced **Generalized Predictive Control** strategy

END